

REPORT No. 837

STANDARD NOMENCLATURE FOR AIRSPEEDS WITH TABLES AND CHARTS FOR USE IN CALCULATION OF AIRSPEED

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SUMMARY

Symbols and definitions of various airspeed terms that have been adopted as standard by the NACA Subcommittee on Aircraft Structural Design are presented. The equations, charts, and tables required in the evaluation of true airspeed, calibrated airspeed, equivalent airspeed, impact and dynamic pressures, and Mach and Reynolds numbers have been compiled. Tables of the standard atmosphere to an altitude of 65,000 feet and a tentative extension to an altitude of 100,000 feet are given along with the basic equations and constants on which both the standard atmosphere and the tentative extension are based.

INTRODUCTION

In analyses of aerodynamic data very often wind-tunnel or flight measurements must be converted into airspeed and related quantities that are used in engineering calculations. Attempts to accomplish such conversion by use of available methods have been complicated by the diversity of symbols and definitions and by the necessity of referring to equations, charts, and tables from a number of different sources. A standard set of symbols and definitions of various airspeed terms that were adopted by the NACA Subcommittee on Aircraft Structural Design and a compilation of the necessary equations, charts, and tables for converting measured pressures and temperatures into airspeeds, determining Mach numbers and Reynolds numbers, and determining other quantities such as dynamic and impact pressures that are of interest are therefore presented herein.

In the preparation of the present paper, results that have been included in previous papers have been extended to include higher altitudes and quantities not given in the previous papers, since recent requests have indicated the need for such an extension of standard-atmosphere tables.

The tables and figures have been arranged for ease in determination of the airspeed, which is usually based on the interpretation of measurements of differential pressures obtained with some pitot-static arrangement. The interrelation of the various airspeed quantities is independent of the method used in the measurement. Instrument and installation errors have been assumed to have been taken into account.

STANDARD SYMBOLS AND DEFINITIONS

At the November 1944 meeting of the NACA Subcommittee on Aircraft Structural Design, representatives from the

Army, Navy, CAA, NACA, and several aircraft manufacturers adopted as standard the following symbols and definitions for airspeeds:

V true airspeed

V_i indicated airspeed (the reading of a differential-pressure airspeed indicator, calibrated in accordance with the accepted standard adiabatic formula to indicate true airspeed for standard sea-level conditions only, uncorrected for instrument and installation errors)

V_c calibrated airspeed (the airspeed related to differential pressure by the accepted standard adiabatic formula used in the calibration of differential-pressure airspeed indicators and equal to true airspeed for standard sea-level conditions)

V_e equivalent airspeed. ($V\sigma^{1/2}$)

Use of equivalent airspeed in combination with various subscripts is customary, particularly in structural design, to designate various design conditions. It is suggested that the foregoing symbols be retained intact when further subscripts are necessary.

Most of the following symbols, which are used herein, have already been accepted as standard and are used throughout aeronautical literature. The units given apply to the development of the equations in the present report.

V true airspeed, feet per second

V_c calibrated airspeed, feet per second

V_e equivalent airspeed, feet per second

a speed of sound in ambient air, feet per second

M Mach number (V/a)

ρ mass density of ambient air, slugs per cubic foot

ρ_0 standard mass density of dry ambient air at sea level, 0.002378 slug per cubic foot

σ density ratio (ρ/ρ_0)

q dynamic pressure, pounds per square foot ($\frac{1}{2}\rho V^2$)

q_c impact pressure, pounds per square foot (total pressure minus static pressure p)

p static pressure of free stream, pounds per square foot

p_0 static pressure of free stream under standard sea-level conditions, pounds per square foot

t temperature, °F or °C

Δt difference between free-air temperature and temperature of standard atmosphere, °F

T	absolute temperature, °F absolute or °C absolute
T_{st}	standard-atmosphere free-air temperature, °F absolute
T_0	standard sea-level absolute temperature, 518.4 °F absolute
T_m	harmonic mean absolute temperature, °F absolute (defined in equation (B5))
f	compressibility factor defined in equation (11)
f_0	compressibility factor defined in equation (16)
γ	ratio of specific heat at constant pressure to specific heat at constant volume (assumed equal to 1.4 for air)
h	absolute altitude, feet
h_p	pressure altitude, feet
g	acceleration of gravity, 32.1740 feet per second per second
m	modulus for common logarithms, $\log_{10} e$ (0.434294)
μ	coefficient of viscosity, slugs per foot-second
ν	kinematic viscosity, square feet per second (μ/ρ)
R	Reynolds number $\left(\rho \frac{Vl}{\mu} \right)$
R_{st}	Reynolds number for standard atmospheric conditions
l	characteristic length, feet

CALCULATION OF AIRSPEED AND RELATED QUANTITIES

Because pitot-static arrangements are used as the basis for the determination of airspeed, aeronautical engineering practice has developed to include the use of a number of airspeed terms and quantities, each of which has a particular field of usefulness. True airspeed is principally of use to aerodynamicists, and indicated and calibrated airspeeds are principally of use to pilots. Equivalent airspeed is used by structural engineers, since all load specifications have long been based on this quantity.

Definite relationships exist between true airspeed, Mach number, Reynolds number, calibrated airspeed, and equivalent airspeed, and all these quantities may be related either to the dynamic pressure q or to the impact pressure q_c . Some of the relations presented herein apply to the calculation of true airspeed and Mach number from airspeed measurements obtained with an airspeed indicator of standard calibration. Other relations apply to the calculation of true airspeed when the impact pressure is measured directly.

If it is assumed that the total-head tube and the static-head tube measure their respective pressures correctly and that these tubes are connected to an appropriate instrument, the impact pressure measured is given by the adiabatic equation when $V < a$:

$$q_c = p \left[\left(1 + \frac{\gamma-1}{2\gamma} \frac{\rho}{p} V^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] \quad (1)$$

Standard airspeed indicators used in Army and Navy airplanes since 1925 have been calibrated according to

equation (1) for standard sea-level conditions; that is, according to the equation when $V < a$,

$$q_c = p_0 \left[\left(1 + \frac{\gamma-1}{2\gamma} \frac{\rho_0}{p_0} V_c^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] \quad (2)$$

where the subscript 0 denotes standard sea-level conditions and V_c is the calibrated airspeed. The calibrated airspeed is, therefore, equal to true airspeed only for standard sea-level conditions.

DETERMINATION OF TRUE AIRSPEED FROM CALIBRATED AIRSPEED

The formula that relates the true airspeed to the calibrated airspeed may be found by equating the right-hand terms of equations (1) and (2) as follows:

$$p \left[\left(1 + \frac{\gamma-1}{2\gamma} \frac{\rho}{p} V^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] = p_0 \left[\left(1 + \frac{\gamma-1}{2\gamma} \frac{\rho_0}{p_0} V_c^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] \quad (3)$$

Because the exact numerical solution of equation (3) for true airspeed is involved and requires a great deal of time, a number of charts for the determination of the true airspeed from the calibrated airspeed for various atmospheric conditions have been derived. (See references 1 to 3.) A typical chart (taken from reference 1) that shows the relationship between Mach number, calibrated airspeed, pressure altitude, temperature, and true airspeed is given in figure 1. This chart is widely used because of its convenience. Airspeed may be obtained from this chart with an accuracy within 2 miles per hour when standard conditions hold and when values of airspeed and pressure altitude explicitly given by the chart are chosen; the possible errors increase to within 5 miles per hour, however, when the temperature conditions are not standard and when interpolation is required for both altitude and airspeed.

For some purposes, charts such as figure 1 are not sufficiently accurate. A series of logarithmic tables that may be used to determine the true airspeed in knots from observed values of calibrated airspeed, pressure altitude, and free-air temperature is given in reference 4. Logarithmic tables of the type given in reference 4 are of limited usefulness since they cannot be used conveniently to evaluate the intermediate quantities (impact pressure and Mach number) that are involved in the computation of true airspeed.

A series of tables (tables I to V) is given in the present report to permit determination of impact pressure q_c in pounds per square foot, Mach number M , and true airspeed V in miles per hour or knots for observed values of V_c in miles per hour or knots, pressure altitude h , in feet, and temperature in degrees Fahrenheit or Centigrade. The accuracy of the tables is far greater than that with which experimental data can normally be obtained. With ordinary care in interpolation, errors should be less than 0.25 mile per hour throughout the greater part of the airspeed and altitude ranges.

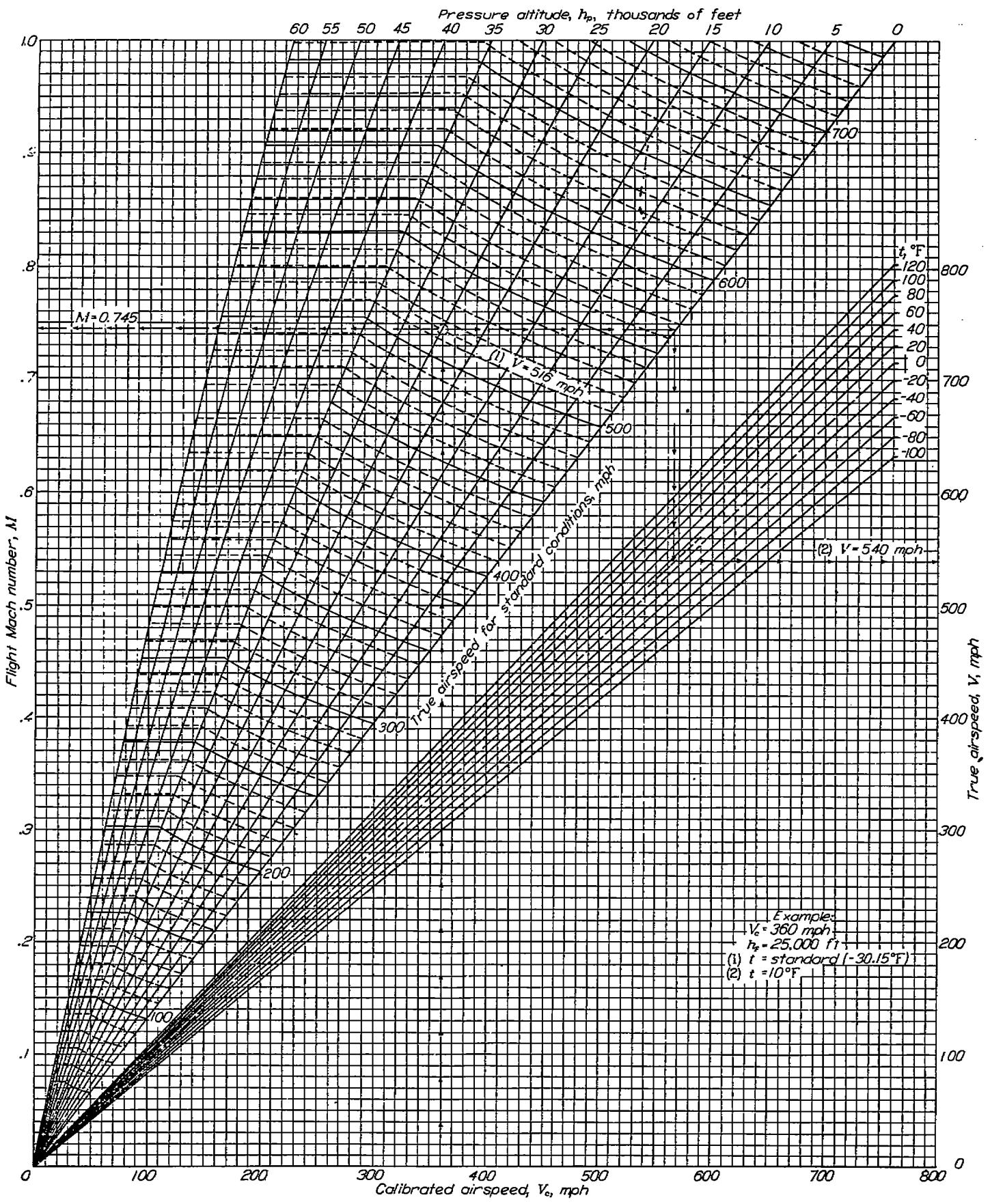


FIGURE 1.—Chart of airspeed against Mach number. (From reference 1.) Airspeed indicator is assumed to be calibrated to read true airspeed for standard sea-level conditions.

Table I, which gives values of impact pressure q_e in pounds per square foot for values of V_e in miles per hour, was computed directly from equation (2); standard values were used for all the constants occurring in this equation. Table II gives values of impact pressure q_e in pounds per square foot for values of V_e in knots. In computing the values of q_e in table II, the conversion from feet to nautical miles used was as follows:

$$1 \text{ nautical mile} = 6080.2 \text{ feet}$$

Tables I and II give the impact pressures for V_e in increments of 1 mile per hour and 1 knot for speeds corresponding to Mach numbers at sea level from 0 to 1.000.

Table III gives values of static pressure p in pounds per square foot for various values of pressure altitude h_p , from -1,000 to 60,000 feet in increments of 100 feet and from 60,000 to 100,000 in increments of 1,000 feet for standard atmospheric conditions. (The use of the term "standard atmosphere" throughout this report includes values for the standard atmosphere up to an altitude of 65,000 feet and for the tentative extension of the standard atmosphere from 65,000 to 100,000 feet.) The values given in table III were computed from the equation

$$h_p = \frac{p_0}{\rho_0 g m} \frac{T_m}{T_0} \log_{10} \frac{p_0}{p} \quad (4)$$

which is given as equation (4) of reference 5 with slightly different symbols.

From tables I or II and III the ratio of impact pressure to static pressure q_e/p may be established and the Mach number, which is a function of this ratio, may then be found. The relation between Mach number and q_e/p may be found from equation (1) as

$$M = \left[5 \left(\frac{q_e}{p} + 1 \right)^{2/7} - 1 \right]^{1/2} \quad (5)$$

Table IV gives values of Mach number for various values of the ratio q_e/p .

The Mach number M is defined as the ratio of the true airspeed to the speed of sound in ambient air and thus, with the Mach number determined, the true airspeed may be found by the use of

$$V = Ma \quad (6)$$

The speed of sound in ambient air is found from the equation

$$a = \sqrt{\gamma \frac{p}{\rho}} \quad (7)$$

which may be rewritten in the following forms when the value of γ is assumed equal to 1.4 and the air is assumed to follow the gas law

$$\rho = \rho_0 \frac{p}{p_0} \frac{T_0}{T} \quad (8)$$

If a is in miles per hour and T is in degrees Fahrenheit absolute

$$a = 33.42 \sqrt{T} \quad (8)$$

If a is in knots and T is in degrees Fahrenheit absolute

$$a = 29.02 \sqrt{T} \quad (8a)$$

If a is in miles per hour and T is in degrees Centigrade absolute

$$a = 44.84 \sqrt{T} \quad (8b)$$

If a is in knots and T is in degrees Centigrade absolute

$$a = 38.94 \sqrt{T} \quad (8c)$$

Table V gives the speed of sound for values of free-air temperature in degrees Fahrenheit, and table VI gives the speed of sound for temperatures in degrees Centigrade. Tables V and VI give the speed of sound both in miles per hour and in knots.

In order to illustrate the use of tables I to VI to determine the true airspeed from calibrated airspeed, the following example is presented:

Given:

Calibrated airspeed $V_e = 398$ miles per hour

Pressure altitude $h_p = 22,000$ feet

Temperature $t = -12^\circ F$

To find:

True airspeed V in miles per hour

Step (1)

From table I, for $V_e = 398$ miles per hour,

$q_e = 433.7$ pounds per square foot

Step (2)

From table III, for $h_p = 22,000$ feet,

$p = 893.3$ pounds per square foot

Step (3)

From these values,

$$\frac{q_e}{p} = \frac{433.7}{893.3} = 0.4855$$

Step (4)

From table IV, for $\frac{q_e}{p} = 0.4855$,

$$M = 0.7736$$

Step (5)

From table V, for $t = -12^\circ F$,

$$a = 706.9 \text{ miles per hour}$$

Step (6)

By use of equation (6),

$$V = Ma = 0.7736 \times 706.9 \text{ miles per hour} \\ = 546.8 \text{ miles per hour}$$

DETERMINATION OF TRUE AIRSPEED FROM IMPACT PRESSURE

In order to convert measurements of impact pressure to true airspeed, the static pressure and the speed of sound must be known. It is convenient first to determine the Mach number from measurements of the impact pressure and the static pressure. Table IV may be used to find the Mach number from the ratio q_e to p and tables V and VI may be used to find the speed of sound for various values of the free-air temperature. The true airspeed may then be determined from equation (6).

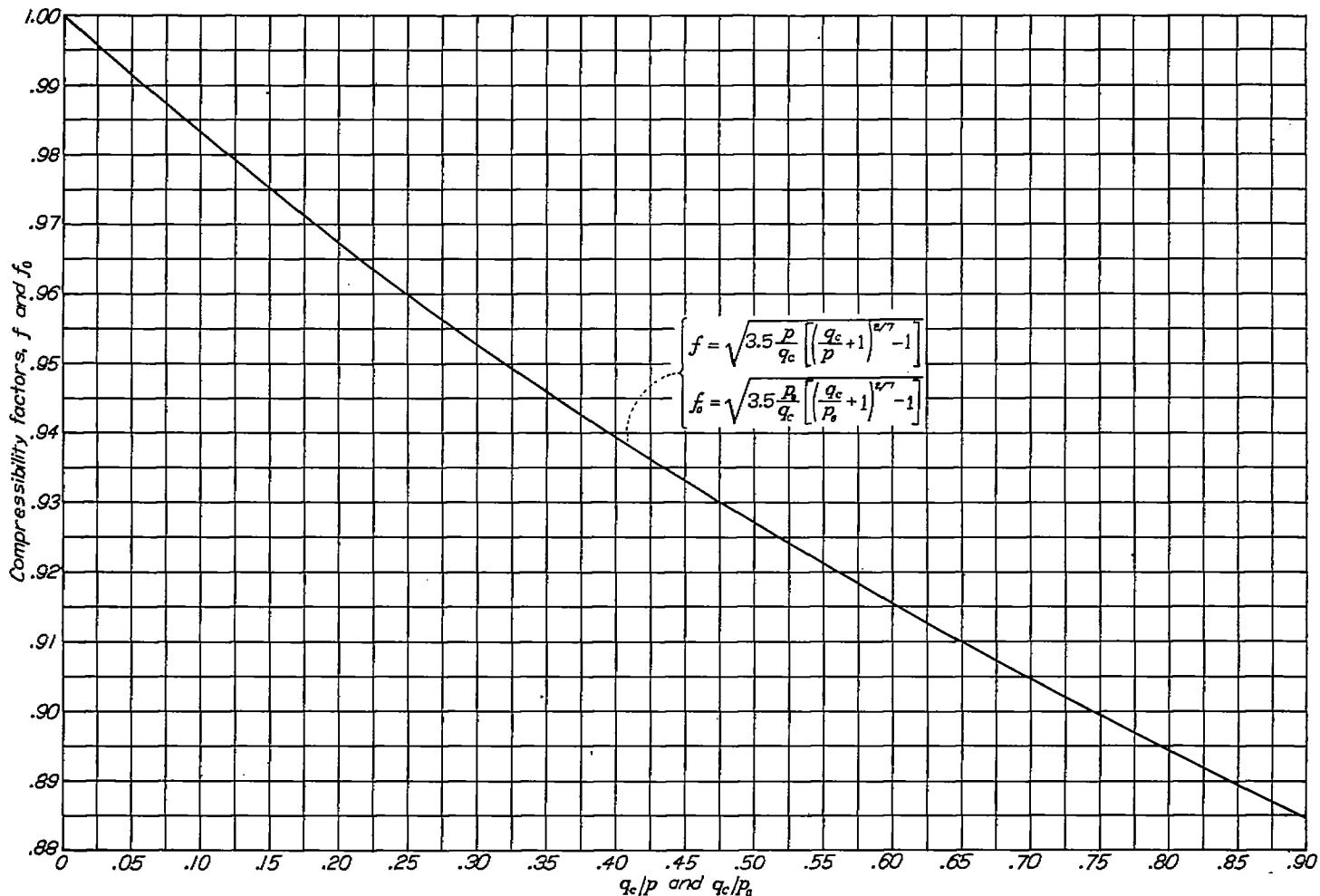


FIGURE 2.—Compressibility factors.

DETERMINATION OF DYNAMIC PRESSURE AND EQUIVALENT AIRSPEED

In order to reduce flight-test data to coefficient form or to demonstrate compliance with certain structural requirements, either the dynamic pressure q or the equivalent airspeed V_e must be determined. The relations of dynamic pressure and equivalent airspeed to impact pressure, static pressure, calibrated airspeed, and Mach number are therefore presented.

Since the dynamic pressure q is by definition

$$q = \frac{1}{2} \rho V^2 \quad (9)$$

it may be expressed as a function of the impact pressure by solving equation (1) for true airspeed and substituting the resultant expression into equation (9), which reduces to

$$q = f^2 q_c \quad (10)$$

where

$$f = \sqrt{\frac{\gamma}{\gamma-1} \frac{p}{q_c} \left[\left(\frac{q_c}{p} + 1 \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} \quad (11)$$

Values of the compressibility factor f are given in figure 2 as a function of q_c/p . The dynamic pressure may also be expressed as a function of Mach number and static pressure from equations (6), (7), and (9) as

$$q = \frac{\gamma}{2} p M^2 \quad (12)$$

Since the equivalent airspeed V_e is by definition

$$V_e = V_{\sigma}^{1/4} = V \sqrt{\frac{p}{p_0}} \quad (13)$$

the relation between the equivalent airspeed in miles per hour, Mach number, and pressure ratio can be derived from equations (6), (8), (13), and the gas-law equation as

$$V_e = 760.9 M \sqrt{\frac{p}{p_0}} \quad (14)$$

The variation, determined from equation (14), of equivalent airspeed with Mach number for pressure altitudes from 0 to 100,000 feet is given in figure 3. For convenience, the true airspeed that applies to the standard atmosphere computed from equations (13) and (14) is also included in figure 3.

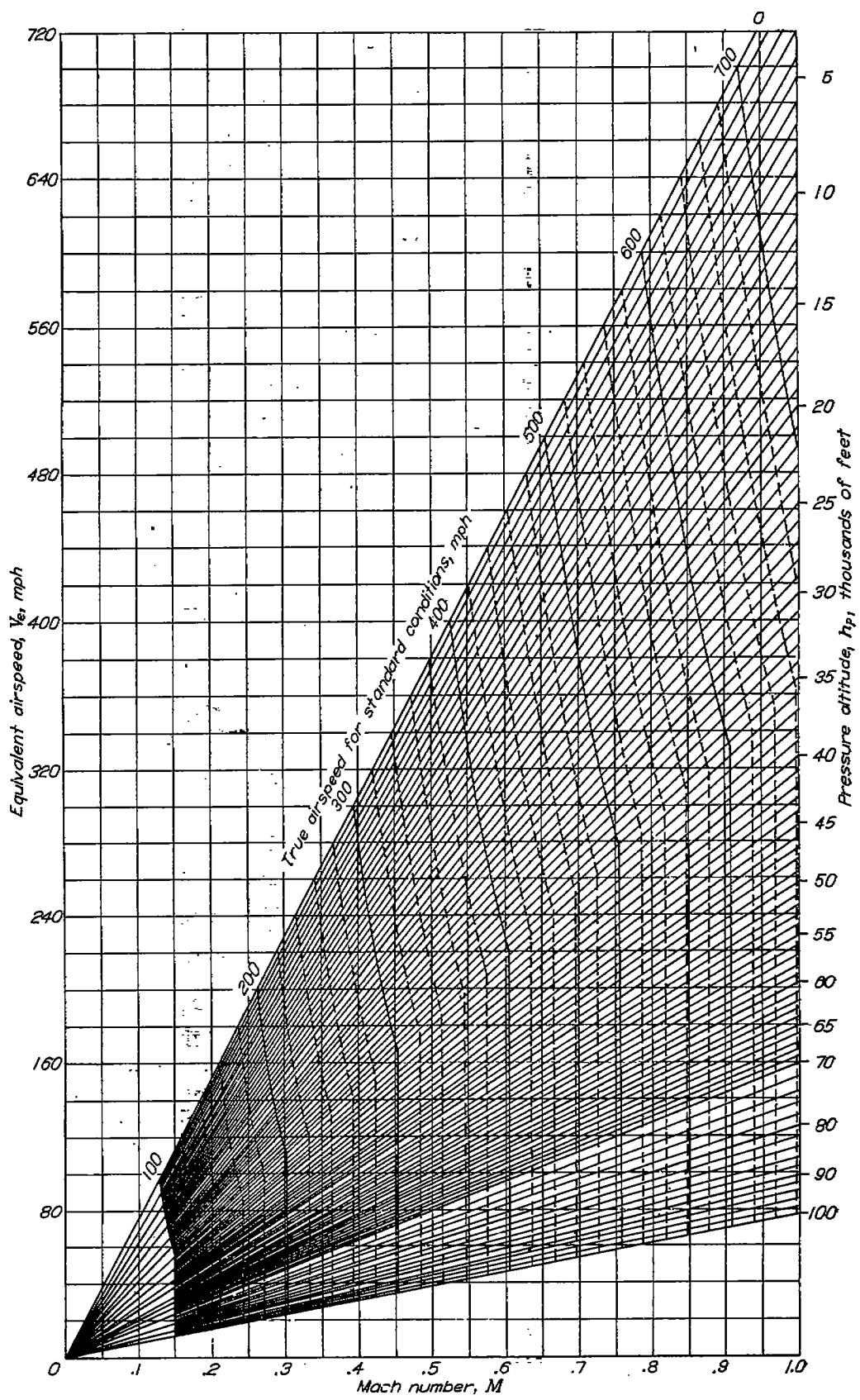


FIGURE 8.—Variation of equivalent airspeed with Mach number and pressure altitude

Finally, expressions that will relate the true airspeed, the calibrated airspeed, and the equivalent airspeed are determined. If equation (2) is solved for V_c :

$$V_c = \sqrt{\frac{\gamma}{\gamma-1} \frac{p_0}{q_c} \left[\left(\frac{q_c}{p_0} + 1 \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} \sqrt{\frac{2q_c}{p_0}} \quad (15)$$

If

$$\sqrt{\frac{\gamma}{\gamma-1} \frac{p_0}{q_c} \left[\left(\frac{q_c}{p_0} + 1 \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} = f_0 \quad (16)$$

equation (15) becomes

$$V_c = f_0 \sqrt{\frac{2q_c}{p_0}} \quad (17)$$

The compressibility factor f_0 is given in figure 2 as a function of q_c/p_0 . Similarly, the true airspeed may be written.

$$V = f \sqrt{\frac{2q_c}{\rho}} \quad (18)$$

From equations (17) and (18)

$$V = V_c \frac{f}{f_0} \sqrt{\frac{p_0}{\rho}} \quad (19)$$

When equations (13) and (19) are summarized

$$V = V_c \frac{f}{f_0} \sqrt{\frac{p_0}{\rho}} = V_e \sqrt{\frac{p_0}{\rho}} \quad (20)$$

For convenience, equations relating the various airspeed quantities are listed in appendix A.

DETERMINATION OF REYNOLDS NUMBER

In comparisons of flight and wind-tunnel results charts relating the Reynolds number to the Mach number have been found convenient.

Reynolds number is defined by the formula

$$R = \frac{Vl\rho}{\mu} = \frac{Vl}{\nu} \quad (21)$$

where l is a characteristic length such as the chord. Equation (21) may be written so that the Reynolds number is expressed as a function of Mach number and absolute temperature in degrees Fahrenheit for unit values of the characteristic length l as

$$\frac{R}{l} = \frac{49.02M\sqrt{T}}{\nu} \quad (22)$$

In order to facilitate the determination of Reynolds number, figure 4 has been prepared to show the variation of the factor R_{std}/l with Mach number and pressure altitude, where R_{std} is the Reynolds number computed on the basis of the

standard atmosphere. Figure 4 (a) holds for pressure altitudes from sea level to 60,000 feet, and figure 4 (b) holds for pressure altitudes from 60,000 to 100,000 feet.

In order to account for free-air conditions other than standard, figure 5 is given to be used in conjunction with figure 4.

When $\mu = \frac{2.318}{10^8} \frac{T^{3/2}}{T+216}$ (justification for the use of this equation given in the section entitled "Properties of Standard Atmosphere") is substituted into equation (21), the Reynolds number factor may be written

$$\frac{R}{l} = 1.232pM \frac{T+216}{T^2} 10^6 \quad (23)$$

The Reynolds number factor in the standard atmosphere becomes

$$\frac{R_{std}}{l} = 1.232pM \frac{T_{std}+216}{T_{std}^2} 10^6 \quad (24)$$

When equation (23) is divided by equation (24)

$$\frac{R}{R_{std}} = \left(\frac{T_{std}}{T} \right)^2 \left(\frac{T+216}{T_{std}+216} \right) \quad (25)$$

Figure 5 gives R/R_{std} as a function of pressure altitude and the deviation Δt of the free-air temperature from standard temperature for a given pressure altitude. In equation form,

$$\Delta t = T - T_{std} \quad (26)$$

The curves of figure 5 become straight lines for pressure altitudes above 35,332 feet, since T_{std} is constant above this altitude range.

In order to illustrate the procedure to be used in determining Reynolds number, the following example is presented: Given:

Mach number $M=0.75$

Pressure altitude $h_p=35,000$ feet

Characteristic length $l=10$ feet

Deviation of free-air temperature from standard temperature $\Delta t=-10^\circ F$

To find:

Reynolds number R

Step (1)

From figure 4 (a), for $M=0.75$ and $h_p=35,000$ feet,

$$\frac{R_{std}}{l} = 1,800,000 \text{ per foot}$$

Step (2)

For $l=10$ feet,

$$R_{std} = 18,000,000$$

Step (3)

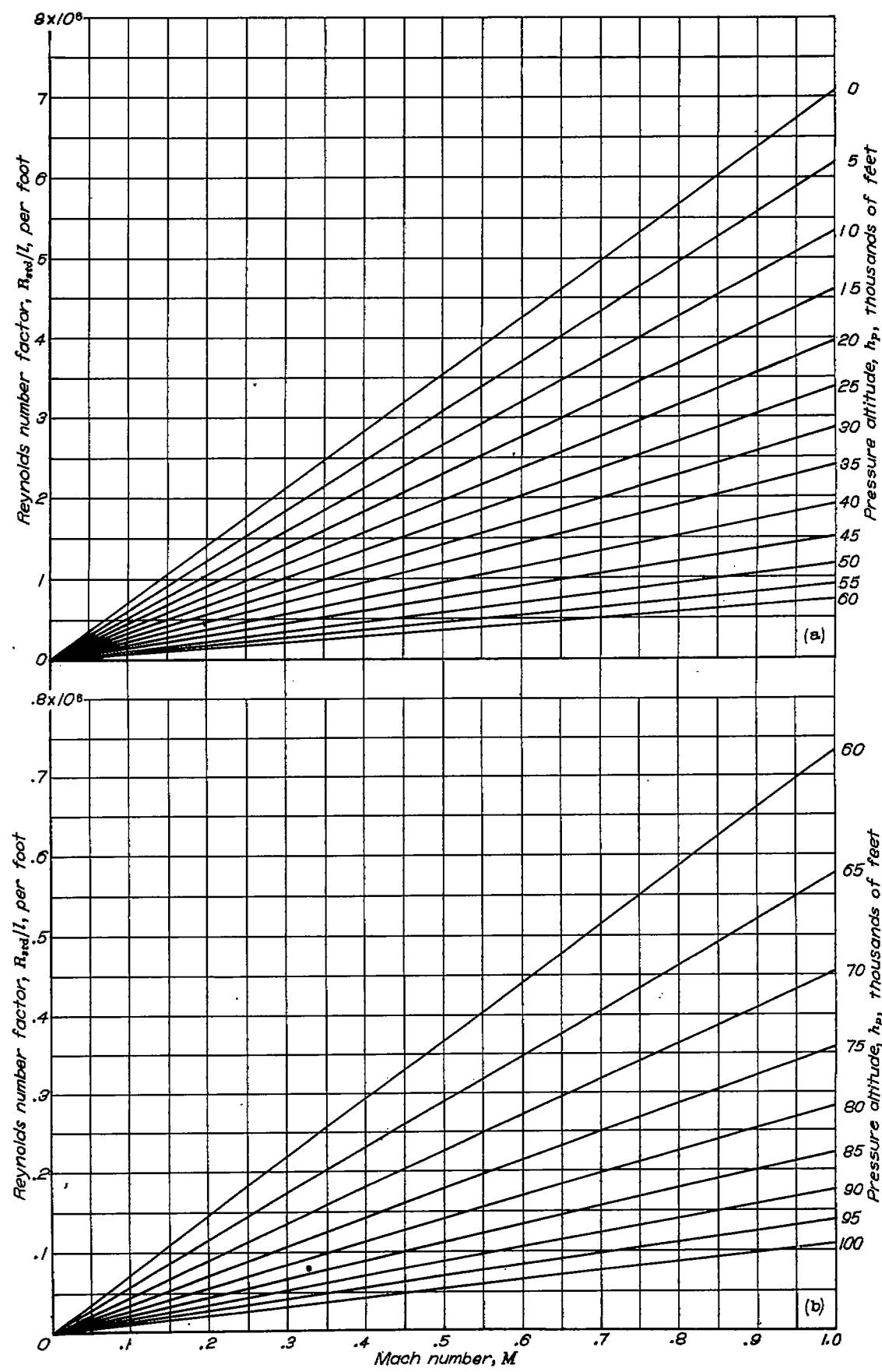
From figure 5, for $h_p=35,000$ feet and $\Delta t=-10^\circ F$,

$$\frac{R}{R_{std}} = 1.036$$

Step (4)

From these values,

$$R = 18,600,000$$



(a) Pressure altitudes from 0 to 60,000 feet.

(b) Pressure altitudes from 60,000 to 100,000 feet.

FIGURE 4.—Variation of Reynolds number factor in the standard atmosphere.

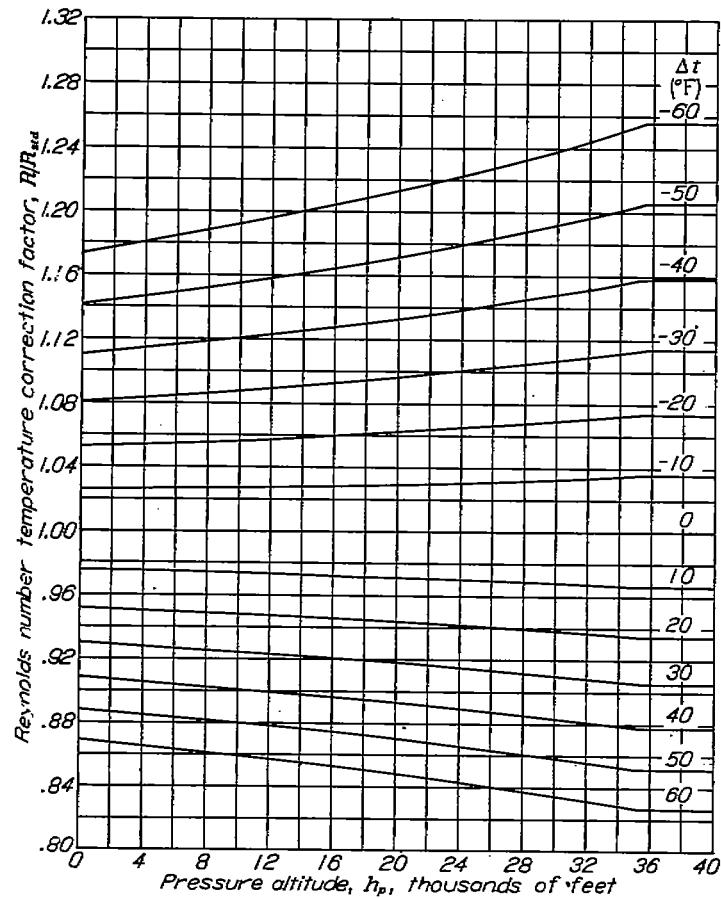


FIGURE 5.—Variation of Reynolds number temperature correction factor with pressure altitude and the deviation Δt of the free-air temperature from the temperature of the standard atmosphere.

PROPERTIES OF STANDARD ATMOSPHERE

For many purposes, such as performance and load calculations, the concept of a standard atmosphere has proved to be very useful. The United States standard atmosphere was officially adopted in 1925 (reference 6). In reference 6 tables are given that are of most use in the calibration of instruments. The properties of this atmosphere were originally tabulated by Diehl (reference 5).

Table VII gives the standard atmospheric values up to altitudes of 65,000 feet and includes quantities that have been found to be of use in the interpretation of airspeed and related factors. These quantities are the pressure in pounds per square foot, the pressure in inches of water, the speed of sound, the coefficient of viscosity μ , and the kinematic viscosity ν . All the quantities given in table VII are in the English system of units for every 500 feet of altitude up to 65,000 feet.

The values given in table VII for the coefficient of viscosity μ and the kinematic viscosity ν are not standard values since a standardization of air viscosity has not been agreed upon as yet. The values listed for μ and ν are believed to be sufficiently accurate, however, to be useful in calculations requiring viscosity of air.

For altitudes from sea level to 35,000 feet, the pressure p

in pounds per square foot and in inches of water was determined from the ratio p/p_0 given in reference 5 and values of the pressure at sea level of 2116.2 pounds per square foot and 407.1 inches of water. The sea-level pressure in pounds per square foot is based on the pressure in inches of mercury at 32° F of 29.921. The sea-level pressure in inches of water is based on the pressure in inches of mercury at 32° F and water at 59° F. The pressure p in inches of mercury for altitudes up to 35,000 feet is taken directly from reference 5.

The quantities mass density ρ and density ratio σ are also taken directly from reference 5 for the altitudes from 0 to 35,000 feet. For altitudes over 35,000 feet the pressures, the mass density, and the density ratio were recalculated, since a minor error was discovered in the calculations of reference 5 for the pressure ratio for altitudes above 35,332 feet.

The quantity $1/\sqrt{\sigma}$ is given to facilitate the computation of the true airspeed V from the equivalent airspeed V_e .

The absolute temperature in degrees Fahrenheit was obtained from reference 5 except for altitudes above 32,000 feet, where interpolation was necessary at the 500-foot stations.

For ready reference, the standard values and the variation with altitude of temperature and density originally used in the computations for the standard atmosphere are included in appendix B of the present paper.

The speed of sound in miles per hour computed from equation (8) is given in table VII. A value of $\gamma=1.4$ was assumed to hold for the temperature range that is included in table VII.

The coefficient of viscosity μ was computed from the formula

$$\mu = \frac{2.318}{10^8} \frac{T^{3/2}}{T+216} \quad (27)$$

Equation (27) was obtained from reference 7 by converting the equation given therein to the English system of units and by starting with a value of $\mu=3.725 \times 10^{-7}$ consistent with the standard sea-level conditions.

The kinematic viscosity of air ν was obtained from the definition

$$\nu = \frac{\mu}{\rho} \quad (28)$$

TENTATIVE EXTENSION OF STANDARD ATMOSPHERE

The NACA Special Subcommittee on the Upper Atmosphere at a meeting on June 24, 1946, resolved that the tentative extension of the standard atmosphere from 65,000 to 100,000 feet be based upon a constant composition of the atmosphere and an isothermal temperature which are the same as standard conditions at 65,000 feet. This tentative extended isothermal region ends at 32 kilometers (approximately 105,000 ft). It is possible that as results of higher altitude temperature soundings become available and the standard atmosphere is extended to very high altitudes the present recommendation may be modified.

The Subcommittee also recommended that the values of temperature given in the following table be considered as maximum and minimum values occurring for the given altitudes with the variations between the specified points to be linear:

Altitude (km)	Temperature (°C abs.)	
	Minimum	Maximum
20	180	250
25	200	250
45	200	380

A tentative extension of the standard atmosphere computed from the equations given in appendix B using the recommended isothermal temperature is given in table VIII for altitudes from 65,000 to 100,000 feet. All quantities given in table VII are included in table VIII.

LANGLEY MEMORIAL AERONAUTICAL LABORATORY,
NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS,
LANGLEY FIELD, VA., July 17, 1946.

APPENDIX A

SUMMARY OF EQUATIONS RELATING AIRSPEED QUANTITIES

The equations relating the various airspeed quantities, which are given in the present paper, are as follows:

$$q_e = p \left[\left(1 + \frac{\gamma-1}{2\gamma} \frac{p}{\rho} V^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] \text{ for } V < a \quad (\text{A1})$$

$$q_e = p_0 \left[\left(1 + \frac{\gamma-1}{2\gamma} \frac{p_0}{\rho_0} V_e^2 \right)^{\frac{\gamma}{\gamma-1}} - 1 \right] \text{ for } V < a \quad (\text{A2})$$

$$q = \frac{1}{2} \rho V^2 \quad (\text{A3})$$

$$q = f^2 q_e \quad (\text{A4})$$

$$q = \frac{\gamma}{2} p M^2 \quad (\text{A5})$$

$$\rho = \rho_0 \frac{p}{p_0} \frac{T_0}{T} \quad (\text{A6})$$

$$f = \sqrt{\frac{\gamma}{\gamma-1} \frac{p}{q_e} \left[\left(\frac{q_e}{p} + 1 \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} \quad (\text{A7})$$

$$f_0 = \sqrt{\frac{\gamma}{\gamma-1} \frac{p_0}{q_e} \left[\left(\frac{q_e}{p_0} + 1 \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} \quad (\text{A8})$$

$$M = \left\{ 5 \left[\left(\frac{q_e}{p} + 1 \right)^{2/7} - 1 \right] \right\}^{1/2} \quad (\text{A9})$$

$$a = \sqrt{\gamma \frac{p}{\rho}} \quad (\text{A10})$$

If a is in miles per hour and T is in degrees Fahrenheit absolute

$$a = 33.42 \sqrt{T} \quad (\text{A11})$$

If a is in knots and T is in degrees Fahrenheit absolute

$$a = 29.02 \sqrt{T} \quad (\text{A12})$$

If a is in miles per hour and T is in degrees Centigrade absolute

$$a = 44.84 \sqrt{T} \quad (\text{A13})$$

If a is in knots and T is in degrees Centigrade absolute

$$a = 38.94 \sqrt{T} \quad (\text{A14})$$

$$V = Ma \quad (\text{A15})$$

$$V = f \sqrt{\frac{2q_e}{\rho}} \quad (\text{A16})$$

$$V_e = f_0 \sqrt{\frac{2q_e}{\rho_0}} \quad (\text{A17})$$

$$V_e = V \sigma^{1/2} = V \sqrt{\frac{p}{\rho_0}} \quad (\text{A18})$$

$$V_e (\text{mph}) = 760.9 M \sqrt{\frac{p}{p_0}} \quad (\text{A19})$$

APPENDIX B

CONSTANTS AND EQUATIONS FOR USE IN COMPUTATIONS OF STANDARD ATMOSPHERE

The values of the standard atmosphere given herein are based on the following values:

$$\begin{aligned}\text{Sea-level pressure } p_0 &= 29.921 \text{ in. Hg} \\ &= 407.1 \text{ in. H}_2\text{O} \\ &= 2116.2 \text{ lb/ft}^2\end{aligned}$$

$$\begin{aligned}\text{Sea-level temperature } t_0 &= 59^\circ \text{ F} \\ \text{Sea-level absolute temperature } T_0 &= 518.4^\circ \text{ F} \\ \text{Sea-level density } \rho_0 &= 0.002378 \text{ slug/ft}^3 \\ \text{Gravity } g &= 32.1740 \text{ ft/sec}^2\end{aligned}$$

$$\text{Temperature gradient } \frac{dT}{dh} = 0.00356617^\circ \text{ F/ft}$$

The altitude of the lower limit of the isothermal atmosphere 35,332 ft

Specific weight of mercury at 32° F = 848.7149 lb/ft³

Specific weight of water at 59° F = 62.3724 lb/ft³

Up to the lower limit of the isothermal atmosphere (-67° F corresponding to 35,332 ft) the temperature is assumed to decrease linearly according to the equation

$$T = T_0 - \frac{dT}{dh} h \quad (\text{B1})$$

Further, the atmosphere is assumed to be a dry perfect gas that obeys the laws of Charles and Boyle, so that the mass density corresponding to the pressure and temperature is

$$\rho = \rho_0 \frac{p}{p_0} \frac{T_0}{T} \quad (\text{B2})$$

In reference 5 the pressure and altitude are related by

$$h = \frac{p_0}{\rho_0 g m} \frac{T_m}{T_0} \log_{10} \frac{p_0}{p} \quad (\text{B3})$$

where m is the modulus for common logarithms, that is,

$$m = \log_{10} e = 0.434294 \quad (\text{B4})$$

The harmonic mean temperature T_m is given by

$$T_m = \frac{\sum \Delta h}{\sum \frac{\Delta h}{T_{av}}} = \frac{\Delta h_1 + \Delta h_2 + \dots}{\frac{\Delta h_1}{T_{av_1}} + \frac{\Delta h_2}{T_{av_2}} + \dots} \quad (\text{B5})$$

where $T_{av_1}, T_{av_2}, \dots$ are the average temperatures for the altitude increments $\Delta h_1, \Delta h_2, \dots$

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TABLE I

IMPACT PRESSURE q_a IN POUNDS PER SQUARE FOOT FOR VARIOUS VALUES OF CALIBRATED AIRSPEED V ,
IN MILES PER HOUR

TABLE II

IMPACT PRESSURE q_e IN POUNDS PER SQUARE FOOT FOR VARIOUS VALUES OF CALIBRATED AIRSPEED V_c IN KNOTS

Calibrated airspeed, V_c (knots)	0	1	2	3	4	5	6	7	8	9
0	0	0.003386	0.01356	0.03053	0.05428	0.08479	0.1221	0.1662	0.2171	0.2747
10	.3392	.4105	.4834	.5732	.6648	.7632	.8634	.9603	1.099	1.225
20	1.357	1.496	1.642	1.795	1.954	2.120	2.294	2.474	2.660	2.854
30	3.054	3.261	3.475	3.696	3.923	4.158	4.399	4.647	4.902	5.163
40	6.432	6.707	6.989	6.278	6.574	6.876	7.186	7.502	7.824	8.154
50	8.491	8.835	9.185	9.542	9.906	10.28	10.66	11.04	11.43	11.83
60	12.24	12.65	13.07	13.49	13.92	14.36	14.81	15.26	15.72	16.19
70	16.66	17.15	17.63	18.13	18.63	19.14	19.65	20.18	20.71	21.24
80	21.75	22.34	22.89	23.45	24.03	24.61	25.19	25.78	26.38	26.99
90	27.60	28.22	28.85	29.48	30.12	30.77	31.42	32.08	32.75	33.43
100	34.11	34.80	35.50	36.20	36.91	37.63	38.35	39.08	39.82	40.57
110	41.32	42.08	42.85	43.63	44.41	45.20	45.99	46.80	47.60	48.42
120	49.24	50.08	50.91	51.76	52.61	53.48	54.34	55.22	56.09	56.98
130	57.87	58.78	59.69	60.61	61.53	62.46	63.40	64.35	65.30	66.26
140	67.22	68.20	69.18	70.18	71.17	72.18	73.18	74.20	75.22	76.26
150	77.30	78.35	79.40	80.46	81.53	82.61	83.69	84.79	85.89	87.00
160	88.11	89.24	90.36	91.50	92.63	93.78	94.94	96.11	97.28	98.46
170	99.65	100.8	102.0	103.2	104.5	105.7	106.9	108.2	109.4	110.6
180	111.9	113.2	114.5	115.8	117.1	118.4	119.7	121.0	122.3	123.6
190	126.0	126.4	127.7	129.1	130.4	131.8	133.2	134.6	136.0	137.4
200	138.8	140.2	141.6	143.1	144.5	146.0	147.4	148.9	150.4	151.9
210	154.4	154.9	156.4	157.9	159.4	161.0	162.5	164.1	165.6	167.2
220	168.8	170.4	172.0	173.5	175.1	176.7	178.4	180.0	181.6	183.2
230	184.9	186.6	188.2	189.9	191.6	193.3	195.0	196.7	198.4	200.2
240	201.9	203.6	205.4	207.2	208.9	210.7	212.4	214.2	216.0	217.8
250	219.6	221.5	223.3	225.2	227.0	228.8	230.7	232.6	234.5	236.4
260	238.3	240.2	242.2	244.1	246.0	248.0	249.9	251.8	253.8	255.8
270	257.8	259.7	261.7	263.7	265.8	267.8	269.8	271.8	273.9	276.0
280	278.0	280.1	282.2	284.3	286.4	288.5	290.6	292.8	294.9	297.1
290	299.2	301.4	303.6	305.8	308.0	310.2	312.4	314.6	316.8	319.1
300	321.3	323.6	325.9	328.1	330.4	332.7	335.0	337.3	339.6	342.0
310	344.3	346.6	349.0	351.4	353.8	356.1	358.5	360.9	363.3	365.7
320	368.1	370.6	373.0	375.4	377.9	380.4	382.9	385.4	387.9	390.4
330	398.0	399.5	398.0	400.6	402.2	405.7	408.3	410.9	413.5	416.1
340	418.7	421.4	424.0	426.6	429.3	432.0	434.6	437.3	440.0	442.7
350	445.4	448.2	450.9	453.6	456.4	459.2	461.9	464.7	467.5	470.3
360	473.1	476.0	478.8	481.6	484.5	487.4	490.2	493.1	496.0	498.9
370	501.8	504.8	507.7	510.7	513.6	516.6	519.6	522.6	525.6	528.6
380	531.6	534.6	537.7	540.8	543.8	546.9	550.0	553.0	556.1	559.2
390	562.4	566.5	568.6	571.8	576.0	578.1	581.3	584.5	587.8	591.0
400	594.2	597.4	600.7	604.0	607.2	610.5	613.8	617.1	620.4	623.8
410	627.1	630.4	633.8	637.2	640.6	644.0	647.4	650.8	654.3	657.8
420	661.2	664.7	669.2	671.6	675.1	678.6	682.2	685.7	689.2	692.8
430	696.4	700.0	703.5	707.1	710.8	714.4	718.0	721.6	725.3	729.0
440	732.6	738.3	740.0	743.8	747.5	751.3	755.0	758.8	762.6	766.4
450	770.2	774.0	777.8	781.6	785.5	789.4	793.2	797.1	801.0	805.0
460	808.9	812.8	816.8	820.8	824.7	828.7	832.7	836.7	840.7	844.8
470	848.8	852.9	857.0	861.1	865.2	869.3	873.4	877.6	881.7	885.8
480	890.0	894.2	898.4	902.6	906.8	911.1	915.4	919.6	923.9	928.2
490	932.6	936.9	941.2	945.6	949.9	954.2	958.6	963.0	967.4	971.9
500	976.3	980.8	985.2	989.7	994.2	998.7	1003	1008	1012	1017
510	1022	1026	1031	1036	1040	1044	1049	1054	1058	1063
520	1068	1073	1078	1082	1087	1092	1096	1101	1106	1111
530	1116	1121	1126	1131	1136	1140	1145	1150	1155	1160
540	1165	1170	1175	1180	1185	1190	1196	1201	1206	1211
550	1216	1221	1226	1231	1236	1242	1247	1252	1258	1263
560	1268	1274	1279	1284	1290	1296	1301	1306	1312	1317
570	1322	1328	1333	1339	1344	1350	1356	1362	1367	1372
580	1378	1384	1389	1394	1400	1406	1412	1417	1423	1429
590	1435	1441	1447	1453	1458	1464	1470	1476	1482	1488
600	1494	1500	1506	1512	1518	1524	1530	1536	1542	1548
610	1554	1560	1566	1572	1578	1585	1591	1597	1604	1610
620	1616	1622	1629	1636	1642	1648	1654	1661	1667	1674
630	1680	1686	1693	1700	1706	1713	1720	1726	1733	1740
640	1746	1753	1760	1766	1773	1780	1786	1793	1800	1807
650	1814	1821	1828	1835	1842	1848	1855	1862	1869	1876
660	1883	1890								

TABLE III

STATIC PRESSURE p IN POUNDS PER SQUARE FOOT FOR VALUES OF
PRESSURE ALTITUDE h , FROM -1,000 TO 100,000 FEET

TABLE IV
MACH NUMBER FOR VARIOUS VALUES OF q_e/p
[For example: at $\frac{q_e}{p} = 0.021$, $M = 0.1725$; at $\frac{q_e}{p} = 0.086$, $M = 0.2254$]

$\frac{q_e}{p}$	0	1	2	3	4	5	6	7	8	9
0	0.0000	0.0377	0.0536	0.0656	0.0757	0.0846	0.0927	0.1001	0.1069	0.1133
.01	.1194	.1282	.1307	.1380	.1411	.1460	.1508	.1554	.1593	.1642
.02	.1684	.1725	.1765	.1804	.1843	.1881	.1918	.1954	.1990	.2025
.03	.2059	.2093	.2126	.2159	.2191	.2227	.2254	.2285	.2315	.2345
.04	.2374	.2403	.2432	.2460	.2488	.2516	.2543	.2570	.2597	.2623
.05	.2649	.2675	.2701	.2726	.2751	.2776	.2801	.2825	.2849	.2873
.06	.2897	.2921	.2944	.2967	.2990	.3013	.3035	.3058	.3080	.3102
.07	.3124	.3146	.3167	.3189	.3210	.3231	.3252	.3273	.3293	.3314
.08	.3334	.3354	.3374	.3394	.3414	.3434	.3453	.3473	.3492	.3511
.09	.3590	.3549	.3568	.3587	.3606	.3624	.3643	.3661	.3679	.3697
.10	.3715	.3733	.3751	.3769	.3786	.3804	.3821	.3839	.3856	.3873
.11	.3890	.3907	.3924	.3941	.3958	.3974	.3991	.4007	.4024	.4040
.12	.4058	.4072	.4089	.4105	.4121	.4137	.4153	.4168	.4184	.4199
.13	.4216	.4231	.4246	.4261	.4277	.4292	.4307	.4322	.4338	.4353
.14	.4367	.4382	.4397	.4412	.4427	.4441	.4456	.4470	.4484	.4499
.15	.4513	.4527	.4542	.4556	.4570	.4584	.4598	.4612	.4626	.4640
.16	.4654	.4668	.4682	.4695	.4709	.4723	.4736	.4750	.4763	.4777
.17	.4790	.4803	.4817	.4830	.4843	.4856	.4869	.4882	.4895	.4908
.18	.4921	.4934	.4947	.4960	.4972	.4985	.4998	.5010	.5023	.5035
.19	.5048	.5060	.5078	.5085	.5098	.5110	.5122	.5135	.5147	.5159
.20	.5171	.5183	.5195	.5207	.5219	.5231	.5243	.5255	.5266	.5278
.21	.5290	.5302	.5313	.5325	.5337	.5348	.5360	.5372	.5383	.5394
.22	.5406	.5417	.5429	.5440	.5452	.5463	.5474	.5485	.5497	.5508
.23	.5519	.5530	.5541	.5552	.5563	.5574	.5585	.5596	.5607	.5618
.24	.5629	.5640	.5651	.5662	.5673	.5683	.5694	.5705	.5716	.5728
.25	.5737	.5748	.5758	.5769	.5779	.5790	.5800	.5811	.5821	.5832
.26	.5842	.5852	.5863	.5873	.5884	.5894	.5904	.5914	.5925	.5935
.27	.5945	.5955	.5965	.5975	.5985	.5995	.6005	.6015	.6025	.6035
.28	.6045	.6055	.6065	.6075	.6084	.6094	.6104	.6114	.6124	.6133
.29	.6143	.6153	.6162	.6172	.6182	.6191	.6201	.6210	.6220	.6229
.30	.6239	.6248	.6258	.6267	.6277	.6286	.6296	.6305	.6314	.6324
.31	.6333	.6342	.6352	.6361	.6370	.6379	.6388	.6398	.6407	.6416
.32	.6426	.6434	.6443	.6452	.6461	.6470	.6479	.6488	.6497	.6506
.33	.6515	.6524	.6533	.6542	.6551	.6560	.6569	.6578	.6586	.6595
.34	.6604	.6613	.6622	.6630	.6639	.6648	.6656	.6665	.6674	.6682
.35	.6691	.6700	.6708	.6717	.6726	.6734	.6742	.6751	.6759	.6768
.36	.6776	.6784	.6793	.6801	.6810	.6818	.6827	.6835	.6843	.6852
.37	.6860	.6868	.6876	.6885	.6893	.6901	.6909	.6918	.6926	.6934
.38	.6942	.6950	.6958	.6966	.6975	.6983	.6991	.6999	.7007	.7015
.39	.7028	.7031	.7039	.7047	.7055	.7063	.7071	.7079	.7087	.7095
.40	.7108	.7111	.7119	.7127	.7135	.7143	.7151	.7159	.7166	.7174
.41	.7182	.7190	.7197	.7205	.7213	.7221	.7228	.7236	.7244	.7251
.42	.7259	.7267	.7274	.7282	.7290	.7297	.7305	.7312	.7320	.7327
.43	.7335	.7343	.7350	.7358	.7365	.7373	.7380	.7388	.7395	.7403
.44	.7410	.7417	.7425	.7432	.7439	.7446	.7454	.7461	.7468	.7476
.45	.7493	.7499	.7508	.7515	.7522	.7529	.7537	.7544	.7551	.7559
.46	.7588	.7593	.7601	.7608	.7615	.7622	.7629	.7637	.7644	.7651
.47	.7628	.7636	.7642	.7649	.7656	.7663	.7670	.7677	.7684	.7691
.48	.7698	.7705	.7712	.7719	.7726	.7733	.7740	.7747	.7754	.7761
.49	.7763	.7775	.7782	.7788	.7795	.7802	.7809	.7816	.7822	.7829
.50	.7836	.7843	.7850	.7857	.7863	.7870	.7877	.7884	.7890	.7897
.51	.7904	.7911	.7917	.7924	.7931	.7938	.7944	.7951	.7958	.7964
.52	.7971	.7978	.7984	.7991	.7998	.8004	.8011	.8017	.8024	.8030
.53	.8037	.8044	.8050	.8056	.8063	.8070	.8076	.8082	.8088	.8096
.54	.8102	.8109	.8115	.8122	.8128	.8135	.8141	.8148	.8154	.8161
.55	.8167	.8173	.8180	.8186	.8192	.8199	.8205	.8211	.8217	.8224
.56	.8230	.8236	.8243	.8249	.8255	.8262	.8268	.8274	.8280	.8287
.57	.8293	.8299	.8305	.8312	.8318	.8324	.8330	.8336	.8343	.8349
.58	.8356	.8361	.8368	.8374	.8380	.8386	.8392	.8399	.8405	.8411
.59	.8417	.8423	.8429	.8435	.8441	.8447	.8453	.8459	.8465	.8471
.60	.8477	.8483	.8489	.8495	.8501	.8507	.8513	.8519	.8525	.8531
.61	.8537	.8543	.8549	.8555	.8561	.8566	.8572	.8578	.8584	.8590
.62	.8596	.8602	.8608	.8614	.8620	.8626	.8632	.8637	.8643	.8649
.63	.8655	.8661	.8667	.8673	.8678	.8684	.8690	.8696	.8701	.8707
.64	.8713	.8719	.8724	.8730	.8736	.8742	.8747	.8753	.8759	.8764
.65	.8770	.8776	.8781	.8787	.8793	.8799	.8804	.8810	.8816	.8821
.66	.8827	.8833	.8838	.8844	.8850	.8855	.8861	.8866	.8872	.8877
.67	.8883	.8888	.8894	.8899	.8905	.8910	.8916	.8922	.8927	.8932
.68	.8938	.8944	.8949	.8955	.8960	.8966	.8971	.8977	.8982	.8988
.69	.8993	.8998	.9004	.9009	.9015	.9020	.9025	.9031	.9036	.9042
.70	.9047	.9052	.9058	.9063	.9069	.9074	.9080	.9085	.9090	.9096
.71	.9101	.9106	.9112	.9117	.9122	.9128	.9133	.9138	.9143	.9149
.72	.9154	.9159	.9165	.9170	.9175	.9181	.9186	.9191	.9196	.9202
.73	.9207	.9212	.9217	.9223	.9228	.9233	.9238	.9243	.9249	.9254
.74	.9259	.9264	.9269	.9275	.9280	.9285	.9290	.9295	.9301	.9306
.75	.9311	.9316	.9321	.9326	.9331	.9336	.9342	.9347	.9352	.9357
.76	.9362	.9367	.9372	.9377	.9383	.9388	.9393	.9398	.9403	.9408
.77	.9413	.9418	.9423	.9428	.9433	.9438	.9443	.9448	.9453	.9458
.78	.9463	.9468	.9473	.9478	.9483	.9488	.9493	.9498	.9503	.9508
.79	.9513	.9518	.9523	.9528	.9533	.9538	.9542	.9547	.9552	.9557
.80	.9562	.9567	.9572	.9577	.9582	.9587	.9592	.9596	.9601	.9606
.81	.9611	.9616	.9621	.9625	.9630	.9635	.9640	.9645	.9649	.9654
.82	.9659	.9664	.9669	.9673	.9678	.9683	.9688	.9693	.9697	.9702
.83	.9707	.9712	.9717	.9722	.9726	.9731	.9736	.9741	.9745	.9750
.84	.9755	.9760	.9764	.9769	.9774	.9778	.9783	.9788	.9793	.9797
.85	.9802	.9807	.9811	.9816	.9821	.9826	.9830	.9835	.9840	.9844
.86	.9849	.9854	.9858	.9863	.9867	.9872	.9877	.9881	.9886	.9890
.87	.9895	.9900	.9904	.9909	.9913	.9918	.9922	.9927	.9932	.9936
.88	.9941	.9946	.9950	.9955	.9960	.9964	.9968	.9973	.9979	.9982
.89	.9987	.9992	.9996	1.0000						

TABLE V

SPEED OF SOUND FOR VARIOUS VALUES OF FREE-AIR TEMPERATURE IN DEGREES FAHRENHEIT

TABLE VI

SPEED OF SOUND FOR VARIOUS VALUES OF FREE-AIR TEMPERATURE IN DEGREES CENTIGRADE

TABLE VII
PROPERTIES OF THE STANDARD ATMOSPHERE

Altitude, ft	Pressure, p			Density, ρ (slugs/ft ³)	Density ratio, $\sigma = \frac{p}{p_0}$	$\frac{1}{\sqrt{\sigma}}$	Temperature, T (°F abs.)	Speed of sound, a (mph)	Coefficient of viscosity, (slugs/ft·sec)	Kinematic viscosity, (ft ² /sec)
	(lb/ft ²)	(in. H ₂ O)	(in. Hg)							
0	2116	407.1	29.92	0.002378	1.0000	1.0000	518.4	760.9	3.725×10^{-7}	1.566×10^{-4}
600	2078	399.8	29.88	.002243	.9855	1.007	516.6	759.6	3.716	1.586
1,000	2041	392.6	29.84	.00209	.9710	1.015	514.8	758.3	3.705	1.604
1,500	2004	385.5	29.80	.002276	.9568	1.022	512.0	757.0	3.685	1.624
2,000	1968	378.5	29.76	.002242	.9428	1.030	511.2	755.7	3.665	1.644
2,500	1932	371.6	29.71	.002209	.9253	1.038	509.5	754.3	3.674	1.663
3,000	1896	364.8	29.67	.002176	.9151	1.045	507.7	753.0	3.664	1.684
3,500	1862	358.2	29.62	.002144	.9015	1.063	505.9	751.7	3.654	1.704
4,000	1828	351.6	29.58	.002112	.8881	1.061	504.1	750.4	3.644	1.725
4,500	1794	345.1	29.53	.002080	.8748	1.069	502.4	749.1	3.633	1.747
5,000	1760	338.7	29.49	.002049	.8616	1.077	500.6	747.7	3.623	1.768
6,000	1728	332.4	29.43	.002018	.8487	1.085	498.8	746.4	3.612	1.788
6,500	1696	326.2	29.38	.001988	.8358	1.094	497.0	745.1	3.602	1.812
7,000	1664	320.1	29.33	.001957	.8232	1.102	495.2	743.7	3.592	1.835
7,500	1633	314.1	29.29	.001928	.8106	1.111	493.4	742.3	3.581	1.857
8,000	1602	308.2	29.24	.001898	.7982	1.119	491.7	741.0	3.571	1.881
8,500	1572	302.4	29.19	.001869	.7859	1.128	489.9	739.7	3.561	1.905
9,000	1542	296.6	29.14	.001840	.7738	1.137	488.1	738.3	3.550	1.929
9,500	1512	291.0	29.08	.001812	.7619	1.146	486.3	737.0	3.540	1.944
10,000	1483	285.4	29.03	.001784	.7501	1.155	484.5	735.6	3.529	1.978
10,500	1455	279.9	28.98	.001756	.7384	1.164	482.7	734.3	3.519	2.004
11,000	1427	274.5	28.91	.001728	.7269	1.173	481.0	732.9	3.508	2.030
11,500	1399	269.2	28.84	.001702	.7154	1.182	479.2	731.6	3.498	2.055
12,000	1372	264.0	28.77	.001675	.7042	1.192	477.4	730.2	3.487	2.082
12,500	1346	258.9	28.70	.001648	.6931	1.201	475.6	728.8	3.476	2.109
13,000	1319	253.8	28.63	.001622	.6821	1.211	473.8	727.5	3.466	2.137
13,500	1293	248.8	28.56	.001596	.6712	1.220	472.0	726.1	3.455	2.165
14,000	1268	243.9	28.49	.001570	.6605	1.230	470.3	724.7	3.445	2.194
14,500	1243	239.1	28.42	.001545	.6499	1.240	468.5	723.4	3.434	2.223
15,000	1218	234.4	28.35	.001520	.6394	1.250	466.7	722.0	3.423	2.252
15,500	1194	229.7	28.28	.001496	.6291	1.261	464.9	720.6	3.413	2.281
16,000	1170	225.1	28.21	.001472	.6189	1.271	463.1	719.2	3.402	2.311
16,500	1146	220.6	28.14	.001448	.6088	1.282	461.3	717.8	3.391	2.342
17,000	1123	216.1	28.07	.001424	.5983	1.292	459.6	716.4	3.380	2.374
17,500	1101	211.8	27.99	.001401	.5881	1.303	457.8	715.0	3.370	2.405
18,000	1078	207.5	27.92	.001378	.5783	1.314	456.0	713.6	3.360	2.438
18,500	1056	203.3	27.84	.001355	.5688	1.325	454.2	712.2	3.348	2.471
19,000	1035	199.1	27.76	.001333	.5583	1.336	452.4	710.8	3.337	2.503
19,500	1014	195.0	27.68	.001311	.5480	1.347	450.6	709.4	3.326	2.537
20,000	992.6	191.0	27.60	.001289	.5418	1.358	448.9	708.0	3.315	2.573
20,500	972.1	187.0	27.52	.001267	.5327	1.370	447.1	706.6	3.305	2.603
21,000	951.9	183.1	27.44	.001246	.5237	1.382	445.3	705.2	3.294	2.644
21,500	932.0	179.3	27.36	.001225	.5148	1.394	443.5	703.8	3.283	2.680
22,000	912.5	175.6	27.28	.001204	.5061	1.406	441.7	702.4	3.272	2.718
22,500	893.3	171.9	27.20	.001183	.4974	1.418	439.9	701.0	3.261	2.756
23,000	874.4	168.2	27.12	.001163	.4889	1.430	438.2	699.6	3.250	2.794
23,500	855.9	164.7	27.04	.001143	.4805	1.443	436.4	698.1	3.239	2.834
24,000	837.7	161.2	26.96	.001123	.4721	1.455	434.6	696.7	3.228	2.874
24,500	819.8	157.7	26.88	.001103	.4640	1.468	432.8	695.3	3.217	2.916
25,000	802.2	154.3	26.80	.001083	.4559	1.481	431.0	693.8	3.206	2.955
25,500	784.9	151.0	26.71	.001065	.4480	1.494	429.2	692.4	3.195	3.000
26,000	767.9	147.7	26.63	.001046	.4401	1.507	427.5	691.0	3.184	3.044
26,500	751.2	144.5	26.54	.001028	.4323	1.521	425.7	689.5	3.173	3.086
27,000	734.8	141.4	26.46	.001010	.4247	1.534	423.9	688.1	3.162	3.131
27,500	718.7	138.3	26.37	.000992	.4171	1.548	422.1	686.6	3.150	3.175
28,000	697.4	135.2	26.29	.000974	.4097	1.562	420.3	685.2	3.139	3.223
28,500	677.1	132.2	26.20	.000957	.4023	1.577	418.5	683.7	3.128	3.268
29,000	657.1	129.3	26.11	.000940	.3951	1.591	416.8	682.3	3.117	3.316
29,500	637.1	126.4	26.02	.000922	.3879	1.606	415.0	680.8	3.106	3.369
30,000	612.4	123.6	25.93	.000906	.3809	1.620	413.2	679.3	3.094	3.415
30,500	585.0	120.8	25.84	.000889	.3740	1.635	411.4	677.9	3.083	3.468
31,000	561.8	118.0	25.74	.000873	.3671	1.650	409.6	676.4	3.072	3.519
31,500	539.9	115.4	25.64	.000857	.3603	1.666	407.8	674.9	3.060	3.570
32,000	517.9	112.8	25.54	.000842	.3537	1.682	406.1	673.4	3.049	3.621
32,500	496.8	110.2	25.44	.000826	.3472	1.697	404.3	672.0	3.038	3.678
33,000	476.7	107.6	25.34	.000810	.3406	1.713	402.5	670.5	3.026	3.736
33,500	456.8	105.2	25.24	.000795	.3343	1.730	400.7	669.0	3.015	3.792
34,000	434.1	102.8	25.14	.000780	.3280	1.746	399.0	667.5	3.004	3.851
34,500	412.7	100.4	25.04	.000765	.3218	1.763	397.2	666.0	2.992	3.911
35,000	390.5	98.03	24.94	.000750	.3158	1.779	395.4	664.5	2.981	3.975

TABLE VII
PROPERTIES OF THE STANDARD ATMOSPHERE—Concluded

Altitude, h (ft)	Pressure, p			Density, ρ (slugs/ft ³)	Density ratio, $\sigma = \frac{\rho}{\rho_0}$	$\frac{1}{\sqrt{\sigma}}$	Tempera- ture, T (°F abs.)	Speed of sound, a (mph)	Coefficient of viscosity, μ (slugs/ft ² sec)	Kinematic viscosity, ν (ft ² /sec)
	0 lb/ft ²	(in. HgO)	(in. Hg)							
35,000	497.6	95.75	7.036	0.000736	0.2098	1.707	398.6	662.0	2.969×10^{-7}	4.034×10^{-6}
35,332	489.8	94.24	6.928	.000727	.3058	1.803	392.4	662.0	2.962	4.073
35,500	485.8	93.51	6.873	.000721	.3034	1.816	392.4	662.0	2.962	4.105
36,000	474.4	91.31	6.711	.000705	.2963	1.827	392.4	662.0	2.962	4.204
36,500	463.2	89.15	6.552	.000688	.2893	1.839	392.4	662.0	2.962	4.306
37,000	452.2	87.04	6.397	.000672	.2824	1.851	392.4	662.0	2.962	4.410
37,500	441.6	85.00	6.247	.000656	.2758	1.904	392.4	662.0	2.962	4.516
38,000	431.1	82.97	6.098	.000640	.2692	1.927	392.4	662.0	2.962	4.625
38,500	421.0	81.01	5.954	.000625	.2629	1.950	392.4	662.0	2.962	4.737
39,000	411.0	79.10	5.813	.000610	.2567	1.974	392.4	662.0	2.962	4.852
39,500	401.3	77.23	5.676	.000596	.2506	1.998	392.4	662.0	2.962	4.969
40,000	391.9	75.44	5.544	.000582	.2448	2.021	392.4	662.0	2.962	5.089
40,500	382.6	73.64	5.412	.000568	.2390	2.045	392.4	662.0	2.962	5.212
41,000	373.6	71.89	5.284	.000555	.2333	2.070	392.4	662.0	2.962	5.338
41,500	364.8	70.18	5.158	.000542	.2278	2.095	392.4	662.0	2.962	5.467
42,000	356.2	68.56	5.038	.000529	.2225	2.120	392.4	662.0	2.962	5.599
42,500	347.8	66.98	4.919	.000516	.2172	2.146	392.4	662.0	2.962	5.735
43,000	339.6	65.34	4.802	.000504	.2120	2.172	392.4	662.0	2.962	5.873
43,500	331.5	63.79	4.688	.000492	.2070	2.198	392.4	662.0	2.962	6.015
44,000	323.7	62.29	4.578	.000480	.2021	2.224	392.4	662.0	2.962	6.161
44,500	316.1	60.82	4.470	.000469	.1974	2.251	392.4	662.0	2.962	6.310
45,000	308.6	59.40	4.365	.000458	.1927	2.278	392.4	662.0	2.962	6.462
45,500	301.3	58.01	4.268	.000448	.1882	2.305	392.4	662.0	2.962	6.618
46,000	294.2	56.63	4.162	.000437	.1838	2.333	392.4	662.0	2.962	6.778
46,500	287.3	55.28	4.063	.000427	.1794	2.361	392.4	662.0	2.962	6.942
47,000	280.5	53.98	3.967	.000417	.1752	2.389	392.4	662.0	2.962	7.110
47,500	273.9	52.72	3.875	.000407	.1711	2.418	392.4	662.0	2.962	7.282
48,000	267.4	51.46	3.782	.000397	.1670	2.447	392.4	662.0	2.962	7.459
48,500	261.1	50.24	3.692	.000388	.1630	2.477	392.4	662.0	2.962	7.640
49,000	255.0	49.06	3.605	.000379	.1592	2.506	392.4	662.0	2.962	7.824
49,500	248.9	47.92	3.522	.000370	.1555	2.536	392.4	662.0	2.962	8.012
50,000	243.1	46.78	3.438	.000361	.1518	2.567	392.4	662.0	2.962	8.206
50,500	237.3	45.67	3.357	.000352	.1482	2.598	392.4	662.0	2.962	8.404
51,000	231.7	44.60	3.276	.000344	.1447	2.628	392.4	662.0	2.962	8.007
51,500	226.3	43.54	3.200	.000336	.1413	2.660	392.4	662.0	2.962	8.816
52,000	220.9	42.52	3.124	.000328	.1379	2.692	392.4	662.0	2.962	9.028
52,500	215.7	41.51	3.051	.000320	.1347	2.725	392.4	662.0	2.962	9.248
53,000	210.6	40.53	2.979	.000313	.1315	2.758	392.4	662.0	2.962	9.470
53,500	205.6	39.57	2.908	.000305	.1284	2.791	392.4	662.0	2.962	9.699
54,000	200.8	38.64	2.840	.000298	.1254	2.824	392.4	662.0	2.962	9.938
54,500	196.1	37.73	2.773	.000291	.1224	2.858	392.4	662.0	2.962	10.17
55,000	191.4	36.84	2.707	.000284	.1195	2.893	392.4	662.0	2.962	10.42
55,500	186.9	35.97	2.644	.000278	.1167	2.927	392.4	662.0	2.962	10.67
56,000	182.5	35.12	2.581	.000271	.1140	2.962	392.4	662.0	2.962	10.93
56,500	178.2	34.29	2.520	.000264	.1113	2.997	392.4	662.0	2.962	11.19
57,000	174.0	33.43	2.461	.000258	.1087	3.033	392.4	662.0	2.962	11.46
57,500	169.9	32.60	2.403	.000252	.1061	3.070	392.4	662.0	2.962	11.74
58,000	165.9	31.79	2.349	.000246	.1036	3.107	392.4	662.0	2.962	12.02
58,500	162.0	31.17	2.291	.000240	.1011	3.145	392.4	662.0	2.962	12.32
59,000	158.1	30.43	2.236	.000235	.09875	3.182	392.4	662.0	2.962	12.61
59,500	154.4	29.71	2.184	.000229	.09643	3.220	392.4	662.0	2.962	12.92
60,000	150.8	29.01	2.132	.000224	.09415	3.259	392.4	662.0	2.962	13.23
60,500	147.2	28.33	2.082	.000218	.09192	3.298	392.4	662.0	2.962	13.55
61,000	143.8	27.66	2.038	.000213	.08976	3.338	392.4	662.0	2.962	13.88
61,500	140.4	27.01	2.000	.000208	.08764	3.378	392.4	662.0	2.962	14.21
62,000	137.1	26.37	1.968	.000203	.08557	3.419	392.4	662.0	2.962	14.56
62,500	133.8	25.74	1.932	.000199	.08355	3.460	392.4	662.0	2.962	14.91
63,000	130.7	25.14	1.848	.000194	.08158	3.501	392.4	662.0	2.962	15.27
63,500	127.6	24.54	1.804	.000189	.07965	3.542	392.4	662.0	2.962	15.64
64,000	124.6	23.95	1.761	.000185	.07777	3.588	392.4	662.0	2.962	16.02
64,500	121.6	23.40	1.720	.000180	.07594	3.629	392.4	662.0	2.962	16.40
65,000	118.7	22.85	1.679	.000176	.07414	3.672	392.4	662.0	2.962	16.80

TABLE VIII
PROPERTIES OF THE TENTATIVE STANDARD-ATMOSPHERE EXTENSION

Altitude, <i>k</i> (ft)	Pressure, <i>p</i>			Density, <i>P</i> (slugs/ft ³)	Density ratio, $\sigma = \frac{P}{P_0}$	$\frac{1}{\sqrt{\sigma}}$	Temperature, <i>T</i> (°F abs.)	Speed of sound, <i>a</i> (mph)	Coefficient of viscosity, (slugs/ft·sec)	Kinematic viscosity, (ft ² /sec)
	(lb/ft ²)	(in. H ₂ O)	(in. Hg)							
65,000	118.7	22.85	1.879	0.000176	0.07414	3.872	392.4	662.0	2.962×10 ⁻⁷	16.80×10 ⁻⁴
66,000	116.0	22.31	1.840	0.000172	0.07240	3.716	392.4	662.0	2.962	17.20
66,000	118.2	21.78	1.801	0.000168	0.07069	3.761	392.4	662.0	2.962	17.62
66,500	110.5	21.27	1.583	0.000164	0.06801	3.807	392.4	662.0	2.962	18.05
67,000	107.9	20.77	1.526	0.000160	0.06739	3.852	392.4	662.0	2.962	18.48
67,500	105.4	20.28	1.490	0.000156	0.06580	3.898	392.4	662.0	2.962	18.93
68,000	102.9	19.80	1.455	0.000153	0.06424	3.945	392.4	662.0	2.962	19.39
68,500	100.5	19.33	1.421	0.000149	0.06273	3.983	392.4	662.0	2.962	19.86
69,000	98.10	18.87	1.387	0.000146	0.06126	4.041	392.4	662.0	2.962	20.34
69,500	95.79	18.43	1.354	0.000142	0.06081	4.089	392.4	662.0	2.962	20.83
70,000	93.53	17.99	1.322	0.000139	0.05839	4.138	392.4	662.0	2.962	21.33
70,500	91.33	17.57	1.291	0.000136	0.05702	4.188	392.4	662.0	2.962	21.85
71,000	89.17	17.16	1.261	0.000132	0.05667	4.238	392.4	662.0	2.962	22.38
71,500	87.06	16.75	1.231	0.000129	0.05435	4.289	392.4	662.0	2.962	22.92
72,000	85.00	16.35	1.202	0.000126	0.05307	4.341	392.4	662.0	2.962	23.47
72,500	82.99	15.97	1.173	0.000123	0.05181	4.393	392.4	662.0	2.962	24.04
73,000	81.04	15.60	1.148	0.000120	0.05060	4.446	392.4	662.0	2.962	24.62
73,500	79.14	15.22	1.119	0.000117	0.04941	4.499	392.4	662.0	2.962	25.21
74,000	77.26	14.86	1.092	0.000115	0.04822	4.554	392.4	662.0	2.962	25.82
74,500	75.44	14.51	1.067	0.000112	0.04710	4.608	392.4	662.0	2.962	26.45
75,000	73.66	14.17	1.042	0.000109	0.04609	4.663	392.4	662.0	2.962	27.09
76,000	71.92	13.84	1.017	0.000107	0.04490	4.719	392.4	662.0	2.962	27.74
76,000	70.23	13.51	9.930	0.000104	0.04385	4.775	392.4	662.0	2.962	28.41
76,500	68.58	13.19	9.694	0.000102	0.04280	4.833	392.4	662.0	2.962	29.10
77,000	66.95	12.88	9.467	0.000094	0.04180	4.891	392.4	662.0	2.962	29.80
77,500	65.38	12.58	9.242	0.0000970	0.04081	4.950	392.4	662.0	2.962	30.52
78,000	63.82	12.28	9.024	0.0000947	0.03984	5.010	392.4	662.0	2.962	31.26
78,500	62.32	11.99	8.811	0.0000926	0.03891	5.070	392.4	662.0	2.962	32.01
79,000	60.85	11.71	8.605	0.0000903	0.03799	5.131	392.4	662.0	2.962	32.79
79,500	59.42	11.43	8.402	0.0000882	0.03710	5.192	392.4	662.0	2.962	33.58
80,000	58.01	11.16	8.202	0.0000861	0.03621	5.255	392.4	662.0	2.962	34.39
80,500	56.64	10.90	8.010	0.0000841	0.03536	5.317	392.4	662.0	2.962	35.22
81,000	55.31	10.64	7.821	0.0000821	0.03453	5.381	392.4	662.0	2.962	36.08
81,500	54.00	10.39	7.636	0.0000802	0.03371	5.446	392.4	662.0	2.962	36.95
82,000	52.72	10.14	7.455	0.0000783	0.03292	5.511	392.4	662.0	2.962	37.84
82,500	51.43	9.904	7.280	0.0000764	0.03214	5.576	392.4	662.0	2.962	38.76
83,000	50.26	9.670	7.106	0.0000746	0.03138	5.645	392.4	662.0	2.962	39.69
83,500	49.08	9.442	6.933	0.0000729	0.03064	5.713	392.4	662.0	2.962	40.65
84,000	47.92	9.219	6.776	0.0000711	0.02992	5.781	392.4	662.0	2.962	41.63
84,500	46.79	9.001	6.616	0.0000695	0.02921	5.851	392.4	662.0	2.962	42.64
85,000	45.68	8.789	6.460	0.0000678	0.02852	5.921	392.4	662.0	2.962	43.67
85,500	44.60	8.582	6.307	0.0000662	0.02783	5.992	392.4	662.0	2.962	44.73
86,000	43.55	8.379	6.158	0.0000646	0.02719	6.064	392.4	662.0	2.962	45.81
86,500	42.52	8.181	6.013	0.0000631	0.02655	6.137	392.4	662.0	2.962	46.92
87,000	41.52	7.983	5.871	0.0000616	0.02592	6.211	392.4	662.0	2.962	48.05
87,500	40.54	7.800	5.733	0.0000602	0.02531	6.288	392.4	662.0	2.962	49.21
88,000	39.59	7.617	5.598	0.0000588	0.02472	6.361	392.4	662.0	2.962	50.40
88,500	38.66	7.436	5.466	0.0000574	0.02414	6.437	392.4	662.0	2.962	51.62
89,000	37.74	7.260	5.335	0.0000560	0.02358	6.515	392.4	662.0	2.962	52.87
89,500	36.84	7.089	5.209	0.0000547	0.02300	6.593	392.4	662.0	2.962	54.14
90,000	35.97	6.921	5.066	0.0000534	0.02246	6.672	392.4	662.0	2.962	55.46
90,500	35.12	6.758	4.987	0.0000521	0.02193	6.752	392.4	662.0	2.962	56.79
91,000	34.30	6.599	4.850	0.0000509	0.02142	6.834	392.4	662.0	2.962	58.16
91,500	33.49	6.443	4.728	0.0000497	0.02091	6.916	392.4	662.0	2.962	59.57
92,000	32.70	6.291	4.624	0.0000485	0.02041	6.999	392.4	662.0	2.962	61.01
92,500	31.93	6.143	4.514	0.0000474	0.01993	7.083	392.4	662.0	2.962	62.49
93,000	31.17	5.998	4.407	0.0000463	0.01946	7.168	392.4	662.0	2.962	64.00
93,500	30.43	5.856	4.304	0.0000452	0.01900	7.254	392.4	662.0	2.962	65.54
94,000	29.72	5.718	4.202	0.0000441	0.01858	7.341	392.4	662.0	2.962	67.13
94,500	29.02	5.583	4.102	0.0000431	0.01812	7.429	392.4	662.0	2.962	68.75
95,000	28.33	5.451	4.006	0.0000421	0.01769	7.519	392.4	662.0	2.962	70.41
95,500	27.66	5.322	3.912	0.0000411	0.01727	7.609	392.4	662.0	2.962	72.11
96,000	27.01	5.197	3.819	0.0000401	0.01687	7.700	392.4	662.0	2.962	73.86
96,500	26.37	5.074	3.729	0.0000391	0.01647	7.792	392.4	662.0	2.962	75.64
97,000	25.75	4.954	3.641	0.0000382	0.01608	7.886	392.4	662.0	2.962	77.47
97,500	25.14	4.827	3.554	0.0000373	0.01570	7.981	392.4	662.0	2.962	79.34
98,000	24.54	4.723	3.471	0.0000364	0.01533	8.077	392.4	662.0	2.962	81.26
98,500	23.97	4.612	3.390	0.0000356	0.01497	8.174	392.4	662.0	2.962	83.22
99,000	23.40	4.503	3.309	0.0000347	0.01461	8.273	392.4	662.0	2.962	85.24
99,500	22.85	4.397	3.231	0.0000339	0.01427	8.371	392.4	662.0	2.962	87.30
100,000	22.31	4.293	3.156	0.0000331	0.01394	8.472	392.4	662.0	2.962	89.41